

# Activation of Periodate by Freezing for the Degradation of Aqueous Organic Pollutants

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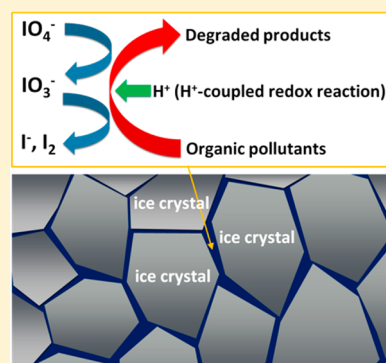
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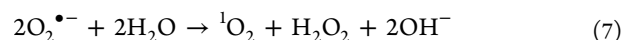
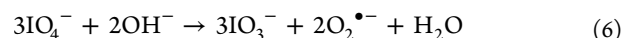
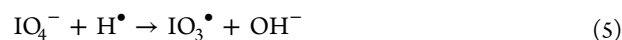
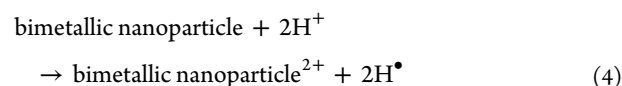
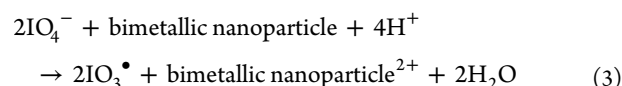
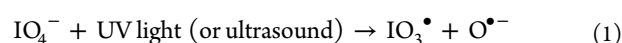
## Supporting Information

**ABSTRACT:** A new strategy (i.e., freezing) for the activation of  $\text{IO}_4^-$  for the degradation of aqueous organic pollutants was developed and investigated. Although the degradation of furfuryl alcohol (FFA) by  $\text{IO}_4^-$  was negligible in water at 25 °C, it proceeded rapidly during freezing at −20 °C. The rapid degradation of FFA during freezing should be ascribed to the freeze concentration effect that provides a favorable site (i.e., liquid brine) for the proton-coupled degradation process by concentrating  $\text{IO}_4^-$ , FFA, and protons. The maximum absorption wavelength of cresol red (CR) was changed from 434 nm (monoprotonated CR) to 518 nm (diprotonated CR) after freezing, which confirms that the pH of the aqueous  $\text{IO}_4^-$  solution decreases by freezing. The degradation experiments with varying experimental parameters demonstrate that the degradation rate increases with increasing  $\text{IO}_4^-$  concentration and decreasing pH and freezing temperature. The application of the  $\text{IO}_4^-$ /freezing system is not restricted to FFA. The degradation of four other organic pollutants (i.e., tryptophan, phenol, 4-chlorophenol, and bisphenol A) by  $\text{IO}_4^-$ , which was negligible in water, proceeded during freezing. In addition, freezing significantly enhanced the  $\text{IO}_4^-$ -mediated degradation of cimetidine. The outdoor experiments performed on a cold winter night show that the  $\text{IO}_4^-$ /freezing system for water treatment can be operated without external electrical energy.



## INTRODUCTION

Inorganic periodate ( $\text{IO}_4^-$ ) has been used for the oxidation of various organic compounds, such as polysaccharides, alginates, amino compounds, and phenolic compounds.<sup>1–5</sup> However, the application of  $\text{IO}_4^-$  as a chemical oxidant for water treatment is limited because the  $\text{IO}_4^-$ -mediated oxidation process is usually very slow. To enhance the oxidation ability of  $\text{IO}_4^-$ , a variety of techniques for  $\text{IO}_4^-$  activation have been employed including a UV/ $\text{IO}_4^-$  system,<sup>6,7</sup> an ultrasound/ $\text{IO}_4^-$  system,<sup>8</sup> a bimetallic nanoparticle/ $\text{IO}_4^-$  system,<sup>9</sup> and a KOH/ $\text{IO}_4^-$  system.<sup>10</sup> Short wavelength UV ( $\lambda \leq 266$  nm) or ultrasound irradiation of  $\text{IO}_4^-$  generates powerful oxidants such as iodyl ( $\text{IO}_3^\bullet$ ) and hydroxyl ( $\bullet\text{OH}$ ) radicals (reactions 1 and 2). The presence of bimetallic nanoparticles ( $\text{Fe}^0/\text{Ni}$  or  $\text{Fe}^0/\text{Cu}$ ) converts  $\text{IO}_4^-$  to  $\text{IO}_3^\bullet$  directly or indirectly through the formation of  $\text{H}^\bullet$  (reactions 3–5). The reaction between  $\text{IO}_4^-$  and  $\text{OH}^-$  produces reactive oxygen species (ROS) such as the superoxide radical ( $\text{O}_2^{\bullet-}$ ) and singlet oxygen ( $^1\text{O}_2$ ) (reactions 6 and 7).



The activation of  $\text{IO}_4^-$  generates powerful oxidants such as  $\text{IO}_3^\bullet$ ,  $\bullet\text{OH}$ ,  $\text{O}_2^{\bullet-}$ , and  $^1\text{O}_2$ , which facilitates the application of  $\text{IO}_4^-$  for

Received: January 16, 2018

Revised: April 11, 2018

Accepted: April 12, 2018

Published: April 12, 2018

water treatment by increasing the degradation rate of aquatic pollutants.

Chemical reactions at temperatures below the freezing point are usually slower than those at temperatures above the freezing point. Therefore, food and unstable chemicals are put in a freezer for long-term storage. However, specific chemical reactions are significantly accelerated during the freezing process due to the existence of thin liquid layer among the solid ice crystals (i.e., ice–ice interface) and on the solid ice crystals (i.e., ice–air interface) at temperatures between the freezing and eutectic points.<sup>11–14</sup> Various terminologies such as liquid brine, ice grain boundary, micropocket have been used to denote this confined liquid layer at temperatures below the freezing point. Solutes and dissolved gases in aqueous solution are expelled from the growing ice crystals and concentrated in the shrinking liquid brine during freezing.<sup>15–17</sup> In addition, protons and hydroxides are accumulated in the liquid brine under acidic and basic conditions, respectively.<sup>18</sup> Therefore, an acidic solution becomes more acidic and a basic solution becomes more basic by freezing. The concentration of solutes, dissolved gases, and protons/hydroxides in the liquid brine during freezing is referred as the “freeze concentration effect”.

This freeze concentration effect during freezing can enhance the chemical reactions in the cold space by increasing the concentrations of reactants and constituting a favorable condition for chemical reactions (i.e., oxygen-rich condition and/or extremely acidic/basic condition). In addition, the reductive/oxidative conversions of pollutants (i.e., chemical reactions between the pollutants or between the pollutants and natural matters) can be accelerated in the cryosphere (e.g., permafrost, polar regions, high-latitudes, and midlatitudes during the winter season). The oxidation rate of nitrite ( $\text{NO}_2^-$ ) to nitrate ( $\text{NO}_3^-$ ) in the presence of oxygen increased by approximately  $10^5$  times upon freezing.<sup>19,20</sup> The redox conversions between chromate ( $\text{Cr}^{6+}$ ) and hydrogen peroxide ( $\text{H}_2\text{O}_2$ )/arsenite ( $\text{As}^{3+}$ )/phenolic pollutants/ $\text{NO}_2^-$ <sup>21–24</sup> were significantly enhanced during freezing. The reduction of bromate ( $\text{BrO}_3^-$ ) by humic substances, which was negligible in water, was clearly observed when the solution was frozen.<sup>25</sup> The N-nitrosation reaction of dimethylamine with  $\text{NO}_2^-$  was significantly accelerated by freezing.<sup>26</sup> Recently, the freezing process was applied to water treatment, in which the  $\text{NO}_2^-$ -mediated oxidation of sulfamethoxazole was significantly accelerated by freezing.<sup>27</sup>

Although various methods for the activation of  $\text{IO}_4^-$  have been developed and applied to the degradation of aquatic pollutants,<sup>6–10</sup> the freezing process has not been tried to activate  $\text{IO}_4^-$ . The term “activation of  $\text{IO}_4^-$ ” usually refers to “the conversion of  $\text{IO}_4^-$  to oxidizing species such as  $\text{IO}_3^\bullet$  and reactive oxygen species”. However, in a broad sense, the term “activation of  $\text{IO}_4^-$ ” in this study has been used to refer to “providing a reaction medium in which  $\text{IO}_4^-$  itself favorably acts as an oxidizing species”. Herein, we report a new strategy for the activation of  $\text{IO}_4^-$  and its application for water treatment, that is, the degradation of aqueous organic pollutants in the presence of  $\text{IO}_4^-$  by freezing. The degradation of organic pollutants with the simultaneous conversion of  $\text{IO}_4^-$  during freezing at  $-20^\circ\text{C}$  was investigated and compared with that in water at  $25^\circ\text{C}$ . The freezing-induced degradation of organic pollutants in the presence of  $\text{IO}_4^-$  was measured as a function of various experimental parameters, such as  $\text{IO}_4^-$  concentration, pH, and freezing temperature. The degradation kinetics of various organic pollutants, such as furfuryl alcohol, cimetidine, tryptophan,

phenol, 4-chlorophenol, and bisphenol A, in the  $\text{IO}_4^-$ /freezing system was compared. Outdoor experiments were performed to verify the practical viability of the  $\text{IO}_4^-$ /freezing system for water treatment (i.e., the energy-free  $\text{IO}_4^-$ /freezing system in cold regions). Furthermore, the degradation mechanism of organic pollutants by  $\text{IO}_4^-$  during freezing is discussed.

## EXPERIMENTAL SECTION

**Chemicals.** All chemicals were used as received without further purification. They include potassium periodate ( $\text{KIO}_4$ , Sigma-Aldrich,  $\geq 99.8\%$ ), potassium iodate ( $\text{KIO}_3$ , Sigma-Aldrich,  $\geq 99.5\%$ ), potassium iodide (KI, Junsei,  $\geq 99.5\%$ ), furfuryl alcohol (FFA,  $\text{C}_5\text{H}_6\text{O}_2$ , Aldrich,  $\geq 98.0\%$ ), tryptophan ( $\text{C}_{11}\text{H}_{12}\text{N}_2\text{O}_2$ , Sigma-Aldrich,  $\geq 98.0\%$ ), cimetidine ( $\text{C}_{10}\text{H}_{16}\text{N}_6\text{S}$ , Sigma, 100%), phenol ( $\text{C}_6\text{H}_5\text{OH}$ , Sigma-Aldrich,  $\geq 99.0\%$ ), 4-chlorophenol ( $\text{ClC}_6\text{H}_4\text{OH}$ , Aldrich,  $\geq 99.0\%$ ), bisphenol A ( $\text{C}_{15}\text{H}_{16}\text{O}_2$ , Aldrich,  $\geq 99.0\%$ ), and cresol red (CR,  $\text{C}_{21}\text{H}_{18}\text{O}_5\text{S}$ , Sigma-Aldrich,  $\geq 95.0\%$ ). All solutions were prepared with ultrapure deionized water (resistivity =  $18.3\text{ M}\Omega\cdot\text{cm}$ ) that was prepared using a Human-Power I+ water purification system (Human Corporation).

**Experimental Procedure.** Aliquots of  $\text{IO}_4^-$  (usually 1 mM, 10 mL) and an organic pollutant (usually FFA, 200  $\mu\text{M}$ , 10 mL) stock solution were added to 80 mL of water in a beaker to yield the desired initial concentration (usually  $[\text{IO}_4^-] = 100\ \mu\text{M}$  and  $[\text{organic pollutant}] = 20\ \mu\text{M}$ ). The pH of the solution (100 mL) was adjusted using a  $\text{HClO}_4$  or  $\text{NaOH}$  solution to the desired value (usually pH 3.0). The solution was unbuffered. Ten mL of this solution was put in a polypropylene conical tube (volume = 15 mL, Nest Biotechnology). The conical tube containing the aqueous solution of  $\text{IO}_4^-$  and organic pollutant was placed in a stainless steel tube rack in a cryogenic ethanol bath, which was precooled to the desired temperature (usually  $-20^\circ\text{C}$ ), to freeze the aqueous solution. The moment that the conical tube containing the aqueous solution was put into the cryogenic ethanol bath was defined as “reaction time zero ( $t = 0$ )”. After reaction in the cryogenic ethanol bath, the conical tube containing the frozen solution was put into a water bath at  $35^\circ\text{C}$  to thaw the frozen solution. The melted solution was immediately analyzed. The experiments in an ethanol bath preset at  $25^\circ\text{C}$  were also performed as the control experiments. Multiple (two or more) experiments were performed for a given condition to confirm data reproducibility.

Outdoor experiments were performed on a vacant lot beside the Natural Science Building in Hallym University (Chuncheon city, Republic of Korea) ( $37^\circ 89' \text{N}$ ,  $127^\circ 47' \text{E}$ ) at night on December 12, 2017. The wind blew lightly. The temperatures during the outdoor experiments were in the range of  $-15 \sim -16^\circ\text{C}$ . Ten mL of aqueous solution containing  $\text{IO}_4^-$  and FFA ( $[\text{IO}_4^-] = 100\ \mu\text{M}$ ,  $[\text{FFA}] = 20\ \mu\text{M}$ , and pH 3.0) was put in a 100 mL beaker. The beaker was set down on the outside ground.

**Chemical Analyses.** The concentrations of organic pollutants, such as FFA, cimetidine, tryptophan, phenol, 4-chlorophenol, and bisphenol A, were measured using high-performance liquid chromatography (HPLC, Agilent 1120) equipped with a UV–visible detector and a Zorbax 300SB C-18 column ( $4.6\text{ mm} \times 150\text{ mm}$ ). The eluent consisted of a binary mixture of 0.1% phosphoric acid solution and acetonitrile, and its flow rate was 1.0 mL/min. The volume ratios (0.1% phosphoric acid solution:acetonitrile) of the eluents and the detection wavelengths were as follows: 85:15 and 218 nm for FFA, 95:5 and 218 nm for cimetidine, 90:10 and 220 nm for tryptophan, 70:30 and 270 nm for phenol, 80:20 and 228 nm for 4-

chlorophenol, and 70:30 and 229 nm for bisphenol A, respectively. The concentration of total organic carbon (TOC) was measured using a TOC analyzer (Shimadzu TOC-L<sub>CPH</sub>) equipped with a nondispersive infrared sensor as a CO<sub>2</sub> detector.

The quantitative analyses of IO<sub>3</sub><sup>-</sup> and I<sup>-</sup> were performed using an ion chromatograph (IC, Dionex ICS-1100) equipped with a Dionex IonPac AS-14 column (4 mm × 250 mm) and a conductivity detector. A binary mixture of 3.5 mM sodium carbonate and 1 mM sodium bicarbonate was used as the eluent at a flow rate of 1.0 mL/min. The concentration of I<sub>2</sub> was determined by measuring the absorbance at 460 nm ( $\epsilon = 746 \text{ M}^{-1} \text{ cm}^{-1}$  at 460 nm)<sup>28</sup> using a UV–visible spectrophotometer (Shimadzu UV-2600). Because the absorbance at 353 nm, which is ascribed to the generation of I<sub>3</sub><sup>-</sup> ( $\epsilon = 26\,400 \text{ M}^{-1} \text{ cm}^{-1}$  at 353 nm and  $\epsilon = 975 \text{ M}^{-1} \text{ cm}^{-1}$  at 460 nm),<sup>28</sup> was negligible (less than 0.0015 (= 0.06  $\mu\text{M}$ ), see Figure S1 in the Supporting Information, SI), only I<sub>2</sub> is responsible for the absorbance at 460 nm.

**pH Estimation of the Frozen Solution.** The pH of the frozen solution was estimated by measuring the UV–visible absorption spectra of cresol red (CR) as an in situ pH probe after freezing, but without thawing (i.e., in the liquid brine).<sup>29,30</sup> 3 mL of an aqueous solution containing IO<sub>4</sub><sup>-</sup> (100  $\mu\text{M}$ ) and CR (20  $\mu\text{M}$ ) in a cylindrical quartz tube (4 mL) was frozen at  $-20 \text{ }^\circ\text{C}$  in a cryogenic ethanol bath and its UV–visible absorption spectrum was immediately recorded using a UV–visible spectrophotometer equipped with a diffuse reflectance accessory (Agilent Cary 5000) after taking the cylindrical quartz tube out from the cryogenic ethanol bath. Nitrogen gas was continuously introduced into the sample compartment to prevent moisture condensation on the cylindrical quartz tube. Pure ice prepared in identical manner was used as a reference.

CR exists in three different forms depending on the pH and exhibits different maximum absorption wavelengths ( $\lambda_{\text{max}} = 518 \text{ nm}$  for diprotonated CR,  $\lambda_{\text{max}} = 434 \text{ nm}$  for monoprotated CR, and  $\lambda_{\text{max}} = 573 \text{ nm}$  for deprotonated CR).<sup>31</sup> However, the three different CR forms cannot coexist in the equilibrium state because there is a great gap between first and second acid dissociation constants ( $\text{p}K_{\text{a}}$ ) of CR ( $\text{p}K_{\text{a}1} = 1.10$  and  $\text{p}K_{\text{a}2} = 8.15$ ).<sup>32,33</sup> Only diprotonated CR and monoprotated CR or monoprotated CR and deprotonated CR can coexist. Therefore, the relative concentrations of the two different CR forms (i.e.,  $[\text{monoprotated CR}]/[\text{diprotonated CR}]$  or  $[\text{deprotonated CR}]/[\text{monoprotated CR}]$ ) can be obtained by fitting the data in the UV–visible absorption spectra of CR to eq 8.<sup>29,30</sup> The non-negative least-squares minimization was performed using Matlab. The pH of frozen solution was calculated according to eq 9 using the relative concentrations of the two different CR forms obtained from eq 8 and the  $\text{p}K_{\text{a}}$  value.

$$\sum_{\lambda=400\text{nm}}^{650\text{nm}} (A \cdot a + B \cdot b - X)^2 = \text{minimum value} \quad (8)$$

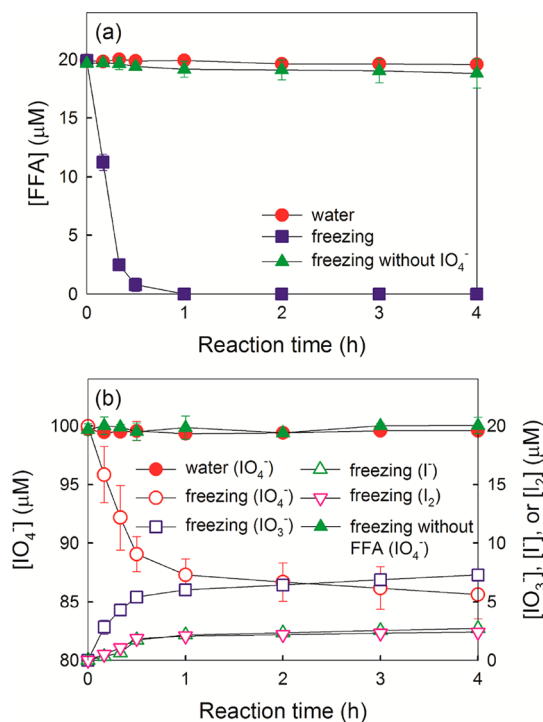
where  $X$  stands for the absorbance of frozen solution,  $A$  and  $B$  stand for the absorbances of pure diprotonated CR and monoprotated CR (or the absorbances of pure monoprotated CR and deprotonated CR), respectively, and  $a$  and  $b$  (non-negative parameters) are the relative concentrations of diprotonated CR and monoprotated CR (or the relative concentrations of monoprotated CR and deprotonated CR), respectively.

$$\text{pH} = \text{p}K_{\text{a}1} + \log \frac{[\text{monoprotated CR}]}{[\text{diprotonated CR}]} \quad (9)$$

$$\left( \text{or } \text{p}K_{\text{a}2} + \log \frac{[\text{deprotonated CR}]}{[\text{monoprotated CR}]} \right)$$

## RESULTS AND DISCUSSION

**Degradation of Furfuryl Alcohol (FFA) by IO<sub>4</sub><sup>-</sup> during Freezing.** The degradation of FFA as a model organic pollutant in the presence of IO<sub>4</sub><sup>-</sup> during freezing at  $-20 \text{ }^\circ\text{C}$  was investigated (Figure 1a). The degradation of FFA by IO<sub>4</sub><sup>-</sup>



**Figure 1.** (a) Degradation of FFA in the presence of IO<sub>4</sub><sup>-</sup> and (b) the concurrent production of IO<sub>3</sub><sup>-</sup>, I<sup>-</sup>, and I<sub>2</sub> in water and during freezing. Experimental conditions were as follows: [IO<sub>4</sub><sup>-</sup>] = 100  $\mu\text{M}$ , [FFA] = 20  $\mu\text{M}$ , pH 3.0, water temperature = 25  $^\circ\text{C}$ , and freezing temperature =  $-20 \text{ }^\circ\text{C}$ .

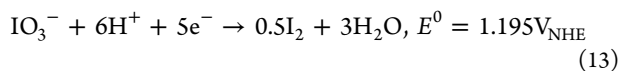
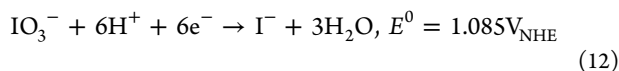
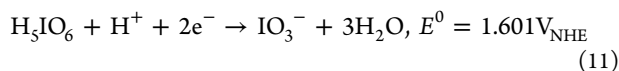
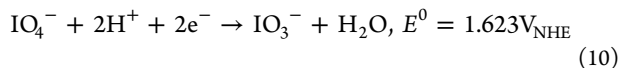
proceeded rapidly during freezing. The degradation of FFA was initiated after 6 min (i.e., when the aqueous solution was almost solidified) (see SI Figures S2 and S3). After 6 min of induction period, the concentration of FFA gradually decreased with the reaction time, and FFA was completely degraded after 1 h of reaction. The mineralization (i.e., the TOC removal) efficiency was 13.5 ( $\pm 1.2$ )% after 4 h of reaction. However, FFA was not degraded by IO<sub>4</sub><sup>-</sup> in water at 25  $^\circ\text{C}$ . In addition, the degradation of FFA during freezing was negligible in the absence of IO<sub>4</sub><sup>-</sup>. The results of the control experiments without either freezing or IO<sub>4</sub><sup>-</sup> indicate that both freezing and IO<sub>4</sub><sup>-</sup> are required for the degradation of FFA.

The degradation of FFA by IO<sub>4</sub><sup>-</sup> during freezing was accompanied by the reduction of IO<sub>4</sub><sup>-</sup> by FFA. The generation of IO<sub>3</sub><sup>-</sup>, I<sup>-</sup>, and I<sub>2</sub> was observed in both the presence of IO<sub>4</sub><sup>-</sup> and FFA during freezing (Figure 1b). The total iodine mass balance was satisfactory throughout the freezing reaction (i.e., reduced [IO<sub>4</sub><sup>-</sup>] = generated [IO<sub>3</sub><sup>-</sup>] + generated [I<sup>-</sup>] + 2 × generated [I<sub>2</sub>]) (see SI Figure S4). This result implies that the missing

iodine species are negligible. In accordance with the results of control experiments for FFA degradation,  $\text{IO}_4^-$  was not reduced in the absence of either FFA or freezing (Figure 1b).

**Activation Mechanism of  $\text{IO}_4^-$  by Freezing.**  $\text{IO}_4^-$  exists in various forms, such as  $\text{H}_5\text{IO}_6$ ,  $\text{H}_4\text{IO}_6^-$ ,  $\text{H}_3\text{IO}_6^{2-}$ ,  $\text{H}_2\text{IO}_6^{3-}$ ,  $\text{IO}_4^-$ , and  $\text{H}_2\text{I}_2\text{O}_{10}^{4-}$ , in water and their molar fraction depends on the pH and the concentration of  $\text{IO}_4^-$  (see SI eqs S1–S5).<sup>34</sup> The speciation of  $\text{IO}_4^-$  can be changed during freezing because the concentration of  $\text{IO}_4^-$  increases and the pH decreases (at acidic conditions) by a freeze concentration effect that accumulates  $\text{IO}_4^-$  and protons in the liquid brine. It was previously estimated that the solute concentration increases by  $10^3$ – $10^6$  times<sup>15</sup> and the pH decreases (at acidic conditions) by 2–4 during freezing.<sup>18</sup> Due to the increase in  $\text{IO}_4^-$  concentration and decrease in pH by freezing, the main iodine<sup>VII</sup> species in water and during freezing can be different. To estimate the main iodine<sup>VII</sup> species in water and during freezing, the pH-dependent speciation of  $\text{IO}_4^-$  was calculated at  $[\text{IO}_4^-] = 100 \mu\text{M}$ , 100 mM, and 100 M using the MINEQL+ chemical equilibrium modeling system (SI Figure S5). Only  $\text{IO}_4^-$  is dominant in water under experimental conditions identical to those of Figure 1 (i.e., at pH 3.0 and  $[\text{IO}_4^-] = 100 \mu\text{M}$ ) (see the results at pH 3.0 in SI Figure S5a). However, both  $\text{IO}_4^-$  and  $\text{H}_5\text{IO}_6$  are expected as a main species during freezing assuming that  $\text{IO}_4^-$  and protons are concentrated in the liquid brine by  $10^3$ – $10^6$  and  $10^2$ – $10^4$  times, respectively (see the results in the pH range of 0–1 in SI Figures S5b and c).

Although  $\text{IO}_4^-$  and  $\text{H}_5\text{IO}_6$  have a fairly high oxidation power (standard reduction potentials ( $E^0$ ) of  $\text{IO}_4^-$  and  $\text{H}_5\text{IO}_6 = 1.623$  and  $1.601 \text{ V}_{\text{NHE}}$ , respectively),<sup>35</sup> protons are essentially required in the degradation process, as shown in reactions 10 and 11. The negligible degradation of FFA by  $\text{IO}_4^-$  in water at pH 3.0 (Figure 1a) implies that 1 mM of protons is not sufficient to drive the degradation of FFA. However, protons are concentrated in the liquid brine by exclusion from ice crystals during freezing, which makes the liquid brine a favorable site for the proton-coupled degradation process (reactions 10 and 11). That is, the degradation of FFA by  $\text{IO}_4^-$  during freezing is most likely due to the pH decrease by the freeze concentration effect. The generation of  $\text{IO}_3^-$  as a product of  $\text{IO}_4^-$  reduction indirectly supports this scenario (see Figure 1b and reactions 10 and 11). Not only  $\text{IO}_3^-$  but also  $\text{I}^-$  and  $\text{I}_2$  were generated during the freezing-induced degradation of FFA in the presence of  $\text{IO}_4^-$  (Figure 1b). This result indicates that  $\text{IO}_3^-$  ( $E^0 = 1.085$  or  $1.195 \text{ V}_{\text{NHE}}$ )<sup>35</sup> generated from  $\text{IO}_4^-$  reduction is also involved in the degradation of FFA during freezing (reactions 12 and 13). When  $\text{IO}_3^-$  was used instead of  $\text{IO}_4^-$ , the degradation of FFA was also observed during freezing (see SI Figure S6).

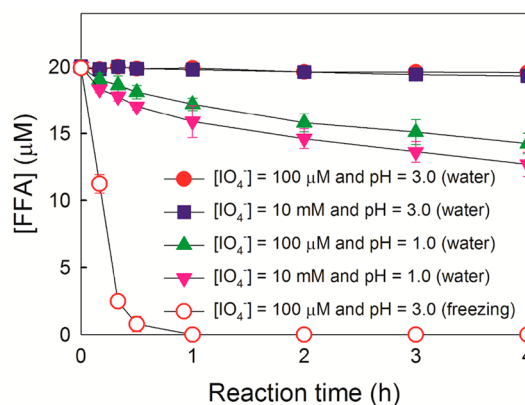


However, the degradation of FFA by  $\text{I}_2$  as well as by  $\text{I}^-$  was negligible both in water and during freezing (SI Figure S7), which indicates that  $\text{I}^-$  and  $\text{I}_2$  generated from  $\text{IO}_3^-$  reduction had little involvement in the degradation of FFA. The one-electron reduction of  $\text{IO}_4^-$  generates  $\text{IO}_3^\bullet$ , which is a highly reactive

oxidant ( $\text{IO}_4^- + 2\text{H}^+ + \text{e}^- \rightarrow \text{IO}_3^\bullet + \text{H}_2\text{O}$ ).<sup>9,36</sup> If the one-electron transfer from FFA to  $\text{IO}_4^-$  during freezing is kinetically favored, FFA can be degraded not only through the electron transfer mechanism (reactions 10–13) but also through radical mechanism. However, the  $\text{IO}_3^\bullet$ -mediated degradation of FFA is only conjecture at this point.

To investigate whether the pH of the aqueous  $\text{IO}_4^-$  solution really decreases and how much (if any) does the pH decrease by freezing, the UV–visible absorption spectra of cresol red (CR) as an in situ pH probe were measured before and after freezing the aqueous  $\text{IO}_4^-$  solution containing CR. The maximum absorption wavelength ( $\lambda_{\text{max}}$ ) of CR varies according to the pH-dependent type of CR ( $\lambda_{\text{max}} = 518 \text{ nm}$  for diprotonated CR,  $\lambda_{\text{max}} = 434 \text{ nm}$  for monoprotonated CR, and  $\lambda_{\text{max}} = 573 \text{ nm}$  for deprotonated CR).<sup>31</sup> The maximum absorbance of CR in aqueous  $\text{IO}_4^-$  solution at pH 3.0 was observed at 434 nm (SI Figure S8) because only monoprotonated CR, which exhibits  $\lambda_{\text{max}}$  at 434 nm, exists at pH 3.0 (see SI Figure S9). The  $\lambda_{\text{max}}$  of CR was shifted from 434 to 518 nm (i.e., most monoprotonated CR was changed to diprotonated CR) after freezing (SI Figure S8), which indicates that the pH of aqueous  $\text{IO}_4^-$  solution decreased by freezing. The ratio of [monoprotonated CR] to [diprotonated CR] after freezing was obtained from SI Figure S8 and eq 8 and estimated to be approximately 1 to 7.1 (i.e., [monoprotonated CR]/[diprotonated CR] = 0.14). Based on eq 9, the pH of the frozen  $\text{IO}_4^-$  solution was estimated to be approximately 0.2. The pH decrease from 3.0 to 0.2 by freezing is consistent with the previous result that the pH decreases by 2–4 by freezing.<sup>18</sup>

To provide convincing evidence that supports the activation of  $\text{IO}_4^-$  by the freezing-induced pH decrease, the degradation of FFA in water was investigated at high concentration of  $\text{IO}_4^-$  and/or low pH (Figure 2). The degradation of FFA in water was

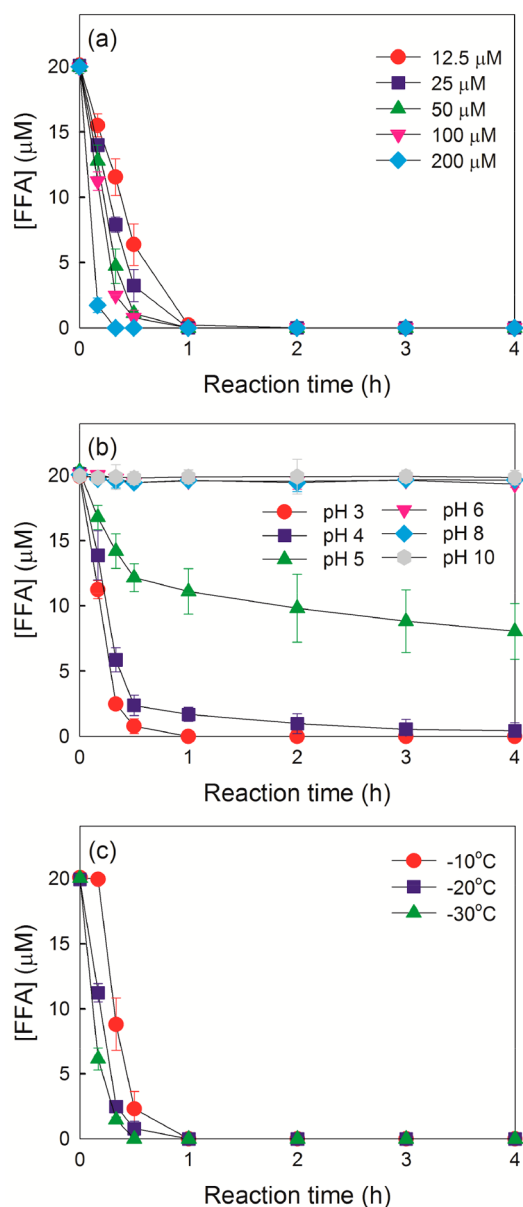


**Figure 2.** Effect of  $\text{IO}_4^-$  concentration increase and/or pH decrease on the degradation of FFA by  $\text{IO}_4^-$  in water. Experimental conditions were as follows:  $[\text{IO}_4^-] = 100 \mu\text{M}$  or  $10 \text{ mM}$ ,  $[\text{FFA}] = 20 \mu\text{M}$ , pH 3.0 or 1.0, water temperature =  $25 \text{ }^\circ\text{C}$ , and freezing temperature =  $-20 \text{ }^\circ\text{C}$ .

negligible at  $[\text{IO}_4^-] = 100 \mu\text{M}$  and pH 3.0. An increase in the  $\text{IO}_4^-$  concentration by 100 times ( $100 \mu\text{M} \rightarrow 10 \text{ mM}$ ) at pH 3.0 also did not induce the degradation of FFA. However, the degradation of FFA in water proceeded when the pH decreased by 2 ( $3.0 \rightarrow 1.0$ ) at  $[\text{IO}_4^-] = 100 \mu\text{M}$ . This result clearly indicates that the pH decrease by freezing is primarily responsible for the degradation of FFA by  $\text{IO}_4^-$ . The degradation of FFA at pH 1.0 was accelerated when the concentration of  $\text{IO}_4^-$  increased by 100 times ( $100 \mu\text{M} \rightarrow 10 \text{ mM}$ ). Overall, the decrease in pH and the increase in the  $\text{IO}_4^-$  concentration in liquid brine by freezing facilitates the proton-coupled degradation processes (reactions

10–13) and enhances the degradation kinetics, respectively. It should be noted that the degradation of FFA during freezing at  $[\text{IO}_4^-] = 100 \mu\text{M}$  and pH 3.0 was much faster than that in water at  $[\text{IO}_4^-] = 10 \text{ mM}$  and pH 1.0 (practically possible limit). This should be because freezing increases the concentrations of  $\text{IO}_4^-$  and protons in the liquid brine much greater than 100 times. In addition, the concentration of FFA in liquid brine should also increase during freezing, which increases the degradation rate of FFA by increasing the chance of contact between  $\text{IO}_4^-$  and FFA.

**Freezing-Induced Degradation of FFA in the Presence of  $\text{IO}_4^-$  under Various Conditions.** The effect of  $\text{IO}_4^-$  concentration, pH, and freezing temperature on the  $\text{IO}_4^-$ -mediated degradation of FFA during freezing was investigated (Figure 3). The degradation of FFA by  $\text{IO}_4^-$  in water was



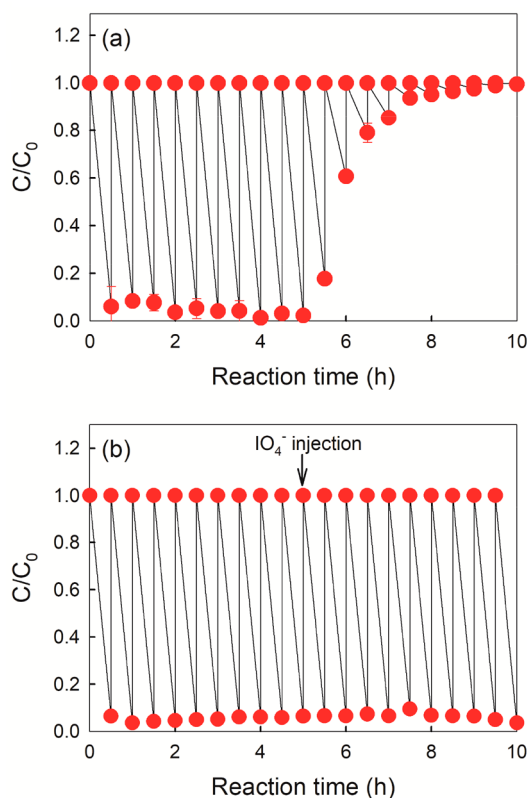
**Figure 3.** Effect of (a)  $\text{IO}_4^-$  concentration, (b) pH, and (c) freezing temperature on the  $\text{IO}_4^-$ -mediated degradation of FFA during freezing. Experimental conditions were as follows:  $[\text{IO}_4^-] = 100 \mu\text{M}$  for parts b and c,  $[\text{FFA}] = 20 \mu\text{M}$ , pH 3.0 for parts a and c, and freezing temperature =  $-20^\circ\text{C}$  for parts a and b.

negligible under experimental conditions identical to those of Figure 3 except for the reaction temperature. The degradation rate of FFA during freezing increased with increasing  $\text{IO}_4^-$  concentration (Figure 3a). Even  $12.5 \mu\text{M}$  of  $\text{IO}_4^-$  completely degraded  $20 \mu\text{M}$  of FFA, which should be ascribed to the fact that  $\text{IO}_3^-$  generated from  $\text{IO}_4^-$  reduction is also involved in the degradation of FFA. All previous methods for the activation of  $\text{IO}_4^-$  (i.e., a UV/ $\text{IO}_4^-$  system, an ultrasound/ $\text{IO}_4^-$  system, a bimetallic nanoparticle/ $\text{IO}_4^-$  system, and a KOH/ $\text{IO}_4^-$  system) require high concentrations of  $\text{IO}_4^-$  because they cannot further activate  $\text{IO}_3^-$  that is generated from  $\text{IO}_4^-$  conversion (the concentration of the degraded pollutant is less than the concentration of added  $\text{IO}_4^-$ ).<sup>6–10</sup> On the other hand, the freezing method can activate not only  $\text{IO}_4^-$  but also  $\text{IO}_3^-$ , which reduces the dose of  $\text{IO}_4^-$  for water treatment (the concentration of the degraded pollutant is higher than the concentration of added  $\text{IO}_4^-$ ).

Figure 3b shows the pH-dependent degradation kinetics of FFA in the presence of  $\text{IO}_4^-$  during freezing. The degradation of FFA was observed below pH 5.0 but was negligible above pH 6.0. The pH of the aqueous  $\text{IO}_4^-$  solution at  $[\text{IO}_4^-] = 100 \mu\text{M}$  and under acidic conditions decreases by 2.8 after freezing (see SI Figure S8 and accompanying discussion). Freezing can reduce the pH from 6.0 to 3.2, which is still an unfavorable condition for the activation of  $\text{IO}_4^-$  (see Figure 2). Therefore, FFA was not degraded during freezing at the acidic pH 6.0. Under basic conditions, hydroxides are accumulated, and the pH increases in the liquid brine by freezing, which constitutes a more unfavorable condition for the proton-coupled degradation process. In the pH range of 3–5, the degradation of FFA by  $\text{IO}_4^-$  during freezing was accelerated as the pH decreased. This behavior is because the lower pH provides a better condition for the proton-coupled degradation process.

We also investigated the effect of freezing temperature on the degradation of FFA by  $\text{IO}_4^-$  (Figure 3c). The degradation rate of FFA increased with decreasing freezing temperature. The generation of  $\text{IO}_3^-$ ,  $\text{I}^-$ , and  $\text{I}_2$  as products of  $\text{IO}_4^-$  and  $\text{IO}_3^-$  reduction was also accelerated with decreasing freezing temperature (SI Figure S10). The concentrations of  $\text{IO}_4^-$ , FFA, and protons in the liquid brine gradually increase with an increase in the size of ice crystals (i.e., with decreasing volume of liquid brine) during freezing. The larger size of ice crystals (i.e., the smaller volume of liquid brine) at lower freezing temperatures produces higher concentrations of  $\text{IO}_4^-$ , FFA, and protons in the liquid brine at any reaction time. Overall, a lower freezing temperature increases the degradation rate of FFA by more rapidly concentrating  $\text{IO}_4^-$ , FFA, and protons in liquid brine.

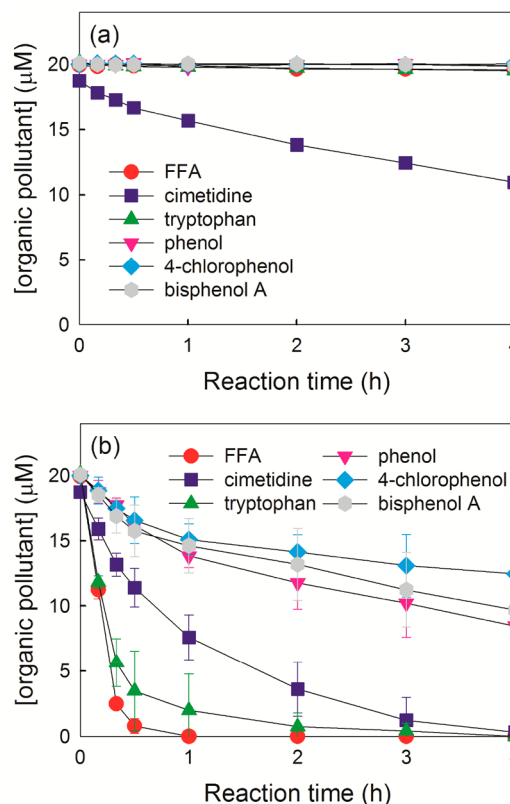
**Applicability of the  $\text{IO}_4^-$ /Freezing System for Water Treatment.** To verify the applicability of the  $\text{IO}_4^-$ /freezing system for water treatment, the freezing-induced degradation of FFA in the presence of  $\text{IO}_4^-$  was repeated up to 20 cycles in the same batch by thawing the frozen sample and injecting FFA every 30 min (Figure 4). When  $\text{IO}_4^-$  ( $100 \mu\text{M}$ ) was added only at the beginning of first cycle, the nearly complete degradation of FFA ( $20 \mu\text{M}$ ) was achieved up to 10 cycles but was reduced from 11th cycle (Figure 4a). Because  $10 \mu\text{M}$  of  $\text{IO}_4^-$  is consumed for the degradation of  $20 \mu\text{M}$  of FFA (see Figure 1),  $100 \mu\text{M}$  of  $\text{IO}_4^-$  should be completely consumed after 10 cycles. Therefore, the reduced degradation efficiency of FFA from 11th cycle should be due to the complete depletion of  $\text{IO}_4^-$ . Although  $\text{IO}_3^-$ ,  $\text{I}^-$ , and  $\text{I}_2$  remain after 10 cycles, only  $\text{IO}_3^-$  can act as an oxidant (see SI Figures S6 and S7). Therefore, the degradation of FFA after 10th cycle (i.e., even in the absence of  $\text{IO}_4^-$ ) should be due to the



**Figure 4.** Repeated cycles of FFA degradation by  $\text{IO}_4^-$  during freezing. FFA was injected at the beginning of each cycle (i.e., every 30 min). For part a,  $\text{IO}_4^-$  was added only at the beginning of first cycle. For part b,  $\text{IO}_4^-$  was additionally injected at the beginning of 11th cycle. Experimental conditions were as follows: initial and injected  $[\text{IO}_4^-] = 100 \mu\text{M}$ , initial and injected  $[\text{FFA}] = 20 \mu\text{M}$ , pH 3.0, and freezing temperature =  $-20^\circ\text{C}$ .

residual  $\text{IO}_3^-$ . However, the additional injection of  $\text{IO}_4^-$  at the beginning of 11th cycle maintained the degradation efficiency of FFA constant up to 20 cycles (Figure 4b). A stable degradation efficiency throughout the repeated cycles before the complete depletion of  $\text{IO}_4^-$  makes the  $\text{IO}_4^-$ /freezing system a practical alternative for water treatment.

We also investigated the degradation of other organic pollutants (i.e., pharmaceutical and phenolic compounds), which are frequently used to evaluate a new water treatment system,<sup>37,38</sup> in the  $\text{IO}_4^-$ /freezing system (Figure 5). Cimetidine and tryptophan were selected as pharmaceutical pollutants. Phenolic pollutants used in this study include phenol, 4-chlorophenol, and bisphenol A. Although the degradation rate of the other organic pollutants during freezing was lower than that of FFA, the degradation of all organic pollutants tested in this study was clearly observed during freezing. The degradation of cimetidine by  $\text{IO}_4^-$  was observed even in water because it is very weak against the electrophilic oxidation (Figure 5a).<sup>10</sup> However, even if that was the case, freezing significantly accelerated the degradation of cimetidine (Figure 5b). The degradation of tryptophan, phenol, 4-chlorophenol, and bisphenol A by  $\text{IO}_4^-$ , which was negligible in water (Figure 5a), continuously proceeded during freezing (Figure 5b). In contrast to the  $\text{KOH}/\text{IO}_4^-$  system that is highly pollutant-specific,<sup>10</sup> the  $\text{IO}_4^-$ /freezing system can be used for the degradation of various organic pollutants. This nonselective degradation ability of the



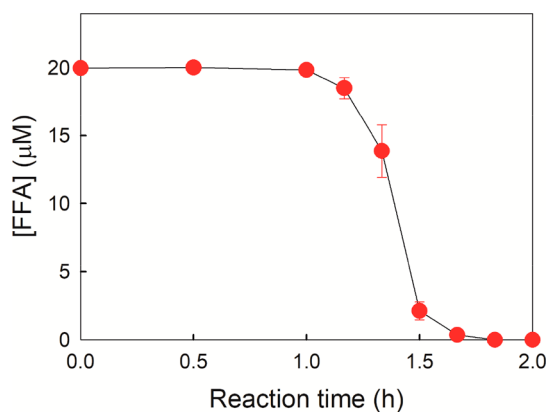
**Figure 5.** Time profiles of the degradation of various organic pollutants (FFA, cimetidine, tryptophan, phenol, 4-chlorophenol, and bisphenol A) by  $\text{IO}_4^-$  (a) in water and (b) during freezing. Experimental conditions were as follows:  $[\text{IO}_4^-] = 100 \mu\text{M}$ ,  $[\text{organic pollutant}] = 20 \mu\text{M}$ , pH 3.0, water temperature =  $25^\circ\text{C}$ , and freezing temperature =  $-20^\circ\text{C}$ .

$\text{IO}_4^-$ /freezing system improves its applicability for water treatment.

To identify which organic pollutant (i.e., chemical structure) is more effectively degraded in the  $\text{IO}_4^-$ /freezing system, the degradation rate of various substituted phenols, such as phenol, 4-chlorophenol, 2-chlorophenol, 2-bromophenol, 2-nitrophenol, 4-nitrophenol, 4-methylphenol, and 2,4-dimethylphenol, was plotted against the Hammett constant ( $\sigma^+$ ), which quantitatively represents the electronic distribution of the substituted phenols. The degradation rates of the substituted phenols decreased with increasing Hammett constant (SI Figure S11). This negative Hammett slope signifies that the degradation of more electron-rich organic pollutants proceeds more rapidly in the  $\text{IO}_4^-$ /freezing system.

The  $\text{IO}_4^-$ /freezing system for water treatment can be operated without external electrical energy in cold regions such as high-latitudes and midlatitudes during the winter season. The freezing-induced degradation of organic pollutants in the presence of  $\text{IO}_4^-$  was tested outdoors without using a cryogenic ethanol bath (external electrical energy) to confirm the energy-free  $\text{IO}_4^-$ /freezing system. The beaker containing the aqueous solution of  $\text{IO}_4^-$  and FFA was only set down on the ground on a cold winter night in the Republic of Korea ( $-15 \sim -16^\circ\text{C}$ ). In contrast to laboratory experiments, which were performed in a cryogenic ethanol bath, an induction period (i.e., the time required for initiation of the degradation process) was clearly observed during the outdoor experiments. This behavior should be due to the difference between cooling methods (the ethanol

cooling system for the laboratory experiments vs an air cooling system for the outdoor experiments, see Discussion on the effect of cooling method on the induction period in the SI for details). The degradation of FFA was started after 1 h and completed within 2 h. (Figure 6). FFA was not degraded in the absence of



**Figure 6.** Degradation of FFA in the presence of  $\text{IO}_4^-$  during freezing (outdoor experiments on a cold winter night in the Republic of Korea). Experimental conditions were as follows:  $[\text{IO}_4^-] = 100 \mu\text{M}$ ,  $[\text{FFA}] = 20 \mu\text{M}$ , pH 3.0, and temperature =  $-15 \sim -16 \text{ }^\circ\text{C}$ .

$\text{IO}_4^-$  under the same conditions. The outdoor experimental results propose that the  $\text{IO}_4^-$ /freezing system for water treatment is economically feasible in cold regions.

The  $\text{IO}_4^-$ /freezing system using the artificial freezing method for wastewater treatment may be impractical, because the electrical costs of freezing a large quantity of wastewater will be too high. However, the practical viability of the  $\text{IO}_4^-$ /freezing system can be established by using a natural freezing method in cold regions, because only  $\text{IO}_4^-$ , which is a cheap reagent, is required in this case. If wastewater containing  $\text{IO}_4^-$  is sprayed in the form of small drops using injection nozzles, the degradation process should be immediately initiated without an induction period due to rapid solidification. This method would make the  $\text{IO}_4^-$ /freezing system for wastewater treatment economically feasible. However, it should be noted that  $\text{I}^-$  in water treated by the  $\text{IO}_4^-$ /freezing system may contribute to the formation of toxic iodine-containing products in the chlorine (or manganese dioxide)-mediated oxidation process.<sup>39,40</sup> Therefore, the subsequent cost-effective methods for the removal of iodide, such as adsorption, precipitation, membrane, and ion-exchange,<sup>41–44</sup> should be employed in conjunction with the  $\text{IO}_4^-$ /freezing system as needed.

We investigated the degradation of aqueous organic pollutants by  $\text{IO}_4^-$  during freezing. Although the degradation of most organic pollutants was negligible in water, it proceeded rapidly during freezing. This unique behavior observed during freezing is due to a freeze concentration effect that provides a favorable site (i.e., liquid brine) for the proton-coupled degradation (i.e., the proton-coupled electron transfer) process by concentrating  $\text{IO}_4^-$ , organic pollutants, and protons in the liquid brine among the ice crystals. The electron transfer from organic pollutants to  $\text{IO}_4^-$  during freezing results in the degradation of organic pollutants accompanied by the production of  $\text{IO}_3^-$ .  $\text{IO}_3^-$  is further converted to  $\text{I}^-$  and  $\text{I}_2$  as a result of electron transfer from organic pollutants to  $\text{IO}_3^-$ . Because freezing can activate not only  $\text{IO}_4^-$  but also  $\text{IO}_3^-$  generated from  $\text{IO}_4^-$  reduction, the freezing method can degrade more organic pollutants than other methods for  $\text{IO}_4^-$  activation at the same  $\text{IO}_4^-$  dose. The degradation

efficiency of the  $\text{IO}_4^-$ /freezing system is stable throughout the repeated cycles before  $\text{IO}_4^-$  is completely depleted. The  $\text{IO}_4^-$ /freezing system can degrade a variety of organic pollutants (i.e., its application is not restricted to a specific pollutant). In particular, the  $\text{IO}_4^-$ /freezing system has the potential to be more economical in cold regions because external electrical energy for freezing is not required.

## ■ ASSOCIATED CONTENT

### Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acs.est.8b00281.

Equations S1–S5, supplementary figures (S1–S11), and discussion on the effect of cooling method on the induction period (PDF)

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### Notes

The authors declare no competing financial interest.

## ■ ACKNOWLEDGMENTS

Funding for this work was provided by the Korea Polar Research Institute (KOPRI) project (PE18200 and PE17560). This research was also supported by Young Research Program (NRF-2016R1A1A1A05005200), Space Core Technology Development Program (NRF-2014M1A3A3A02034875), and Basic Core Technology Development Program for the Oceans and the Polar Regions (NRF-2015M1A5A1037243) through the National Research Foundation of Korea (NRF) funded by the Ministry of Science and ICT.

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