

## RESEARCH ARTICLE

# An automated laser fluorination technique for high-precision analysis of three oxygen isotopes in silicates

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**Rationale:** The three oxygen isotopes in terrestrial/extraterrestrial silicates can provide geochemical and cosmochemical information about their origin and secondary processes that result from isotopic exchange. A laser fluorination technique has been widely used to extract oxygen from silicates for  $\delta^{17}\text{O}$  and  $\delta^{18}\text{O}$  measurements by isotope ratio mass spectrometry. Continued improvement of the techniques is still important for high-precision measurement of oxygen-isotopic ratios.

**Methods:** We adopted an *automated lasing technique* to obtain reproducible fluorination of silicates using a  $\text{CO}_2$  laser- $\text{BrF}_5$  fluorination system connected online to an isotope ratio mass spectrometer. The automated lasing technique enables us to perform high-precision analysis of the three oxygen isotopes of typical reference materials (e.g., UWG2 garnet, NBS28 quartz and San Carlos olivine) and in-house references (mid-ocean ridge basalt glass and obsidian). The technique uses a built-in application of laser control with which the laser power can be varied in a programmed manner with a defocused beam which is in a fixed position.

**Results:** The oxygen isotope ratios of some international reference materials analyzed by the manual lasing technique were found to be isotopically lighter with wider variations in  $\delta^{18}\text{O}$  values, whereas those measured by the automated lasing technique gave better reproducibility (less than 0.2‰, 2SD). The  $\Delta^{17}\text{O}$  values, an excess of the  $\delta^{17}\text{O}$  value relative to the fractionation line, also showed high reproducibility ( $\pm 0.02\%$ , 2SD).

**Conclusions:** The system described herein provides high-precision  $\delta^{17}\text{O}$  and  $\delta^{18}\text{O}$  measurements of silicate materials. The use of the automated lasing technique followed by careful and controlled purification procedures is preferred to achieve satisfactory isotopic ratio results.

## 1 | INTRODUCTION

In 1963, Clayton and Mayeda<sup>1</sup> published a paper on the application of bromine pentafluoride ( $\text{BrF}_5$ ) as a fluorination reagent for the extraction of oxygen from silicate and oxide minerals using a nickel tube with external heating for oxygen isotope analysis. After their historical paper, fluorination-with-laser-heating methods have been developed such as those reported by Sharp,<sup>2</sup> Elsenheimer and

Valley,<sup>3</sup> Miller et al.,<sup>4</sup> Kusakabe et al.,<sup>5</sup> Pack et al.,<sup>6</sup> Ahn et al.,<sup>7</sup> and Tanaka and Nakamura.<sup>8</sup> However, the methods of isotopic analysis are different. The results obtained for a given sample by different authors vary substantially, and there is still disagreement among the reported isotopic data of reference minerals. This is caused by fractionation during extraction procedures adopted in each laser fluorination technique. The possible causes of the variability include (1) the type of laser used, e.g., infrared  $\text{CO}_2$  (wavelength of 10.6  $\mu\text{m}$ )

or Nd:YAG (1064 nm) lasers<sup>3</sup> (2) laser irradiation conditions, e.g., beam diameter and increase rate of output power;<sup>8-10</sup> (3) fluorinating agent (F<sub>2</sub> or BrF<sub>5</sub>) and its purity;<sup>11,12</sup> (4) sample size;<sup>10,13</sup> and (5) design of the sample holder.<sup>14</sup> It is worth emphasizing that fluorination and purification procedures require caution to prevent possible isotopic fractionation during such procedures.

In this study, we describe an infrared CO<sub>2</sub> laser-BrF<sub>5</sub> fluorination system for the analysis of three oxygen isotopes in silicates. We used an automated laser control for lasing silicates in the BrF<sub>5</sub> atmosphere. We measured the three oxygen isotope compositions of five silicate samples; garnet standard at University of Wisconsin (UWG2 garnet), National Bureau of Standard quartz (NBS28 quartz), San Carlos olivine, Juan de Fuca oceanic basalt (JFB) glass, and obsidian as an in-house silicate standard from Coso volcanic field, California, USA, using our improved methods.

## 2 | SYSTEM DESCRIPTION

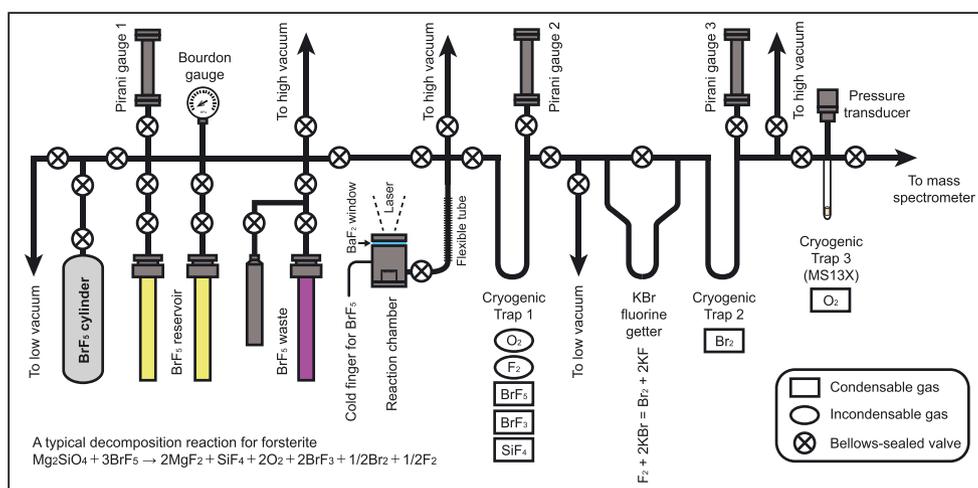
The three oxygen isotope analytical system for silicates using a CO<sub>2</sub> laser-BrF<sub>5</sub> fluorination at the Korea Polar Research Institute (KOPRI, Incheon, Republic of Korea) was installed in 2007 and has been used for the measurement of the oxygen isotopes of terrestrial and extraterrestrial rocks and minerals.<sup>7,15-17</sup> Recently, the system has been replaced completely, with a new metal vacuum line for O<sub>2</sub> extraction and purification. A new mass spectrometer was also introduced. The principle of the system is the same as that described in previous studies.<sup>2,5,7</sup> The laser fluorination system consists of five components (Figure 1); (1) BrF<sub>5</sub> storage and recovery, (2) reaction chamber for laser fluorination, (3) CO<sub>2</sub> laser, (4) purification line, and (5) a gas source isotope ratio mass spectrometer (MAT 253 plus,

Thermo Fisher Scientific, Bremen, Germany). BrF<sub>5</sub> is used as the fluorination reagent. A moderate quantity of BrF<sub>5</sub> is purified by a consecutive freeze-pump-thaw method and transferred into a reagent reservoir made of polychlorotrifluoroethylene (PTFE called Kel-F<sup>®</sup>). The reaction chamber made of stainless steel is sealed by a BaF<sub>2</sub> window (5 mm thick, 50 mm diameter) with a Kalrez<sup>®</sup> O-ring (Figure 2A). The whole reaction chamber is mounted on a motorized X-Y stage and placed under a CO<sub>2</sub> infrared (10.6 μm wavelength) laser system (Universal Laser Systems, Scottsdale, AZ, USA). The laser output power can be adjusted from 0 to 100% of the maximum output of 25 W using a computer control program built into the laser unit. The purification line is made of stainless-steel tubing (SUS316) and metal bellows-sealed valves (SS-4H, Swagelok<sup>®</sup>, Solon, OH, USA). Oxygen transfer and the elimination of impurity gases are monitored by Pirani gauges. The extracted oxygen gas is collected in a glass cryogenic trap that contains a pellet of 13X molecular sieve (trap 3, Figure 1). After desorption of O<sub>2</sub>, the gas pressure is measured using a pressure transducer. Calibration of the pressure transducer will be briefly described later.

## 3 | ANALYTICAL METHODS

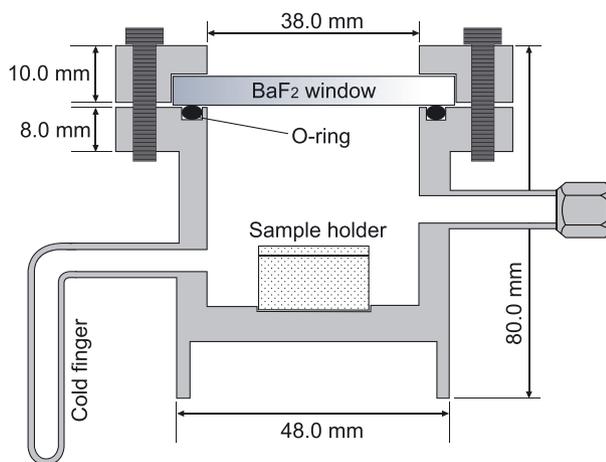
### 3.1 | Laser fluorination and gas purification

Several coarse- or fine-grained silicate samples weighing approximately 2 mg were loaded in a nickel sample holder (Figure 2B), which was placed in the reaction chamber (Figure 2A). The chamber is assembled with the purification line using a metal gasket (VCR<sup>®</sup>, Swagelok<sup>®</sup>), and then evacuated to 10<sup>-3</sup> mbar or better. At the beginning it is heated to 150°C overnight in vacuum with an external heating

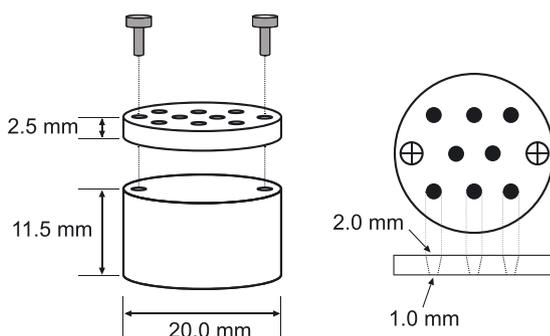


**FIGURE 1** Schematic diagram of the laser fluorination line. Silicates and oxide minerals are heated by a CO<sub>2</sub>-laser in the presence of BrF<sub>5</sub> in the reaction chamber. After the reaction, the excess BrF<sub>5</sub> and product gases such as O<sub>2</sub>, F<sub>2</sub>, BrF<sub>3</sub>, SiF<sub>4</sub>, etc., pass through the purification line. The condensable gases are removed in the first cryogenic traps. Fluorine, which is an incondensable gas at liquid nitrogen temperature (−196°C), reacts with KBr to produce bromine. After that, bromine is trapped in a second cryogenic trap. The purified oxygen gas is collected in the third cryotrap containing a pellet of 13X molecular sieve (MS13X). The gas pressure of the oxygen released from MS13X at room temperature is measured by a pressure transducer to calculate the oxygen yield. The oxygen gas is expanded into the sample bellows of the dual-inlet system of the isotope ratio mass spectrometer for measuring the oxygen isotope ratios [Color figure can be viewed at [wileyonlinelibrary.com](http://wileyonlinelibrary.com)]

## (A) Reaction chamber for laser fluorination



## (B) Nickel sample holder



**FIGURE 2** Schematic diagram of A, reaction chamber and B, nickel sample holder with dimensions. The sample holder consists of top and bottom parts. The top part has eight tapered (cone-shaped) holes having an upper diameter of 2 mm and a lower diameter of 1 mm. It is fixed on the bottom holder by two screws. This sample holder design is advantageous for washing and cleaning after an experiment. The sample holder filled with approximately 2 mg of the sample on each hole is placed in the reaction chamber made of stainless steel, and the reaction chamber is then sealed by a transparent BaF<sub>2</sub> window with a Kalrez O-ring [Color figure can be viewed at [wileyonlinelibrary.com](http://wileyonlinelibrary.com)]

jacket to remove adsorbed atmospheric moisture. Before sample analysis, a small amount of BrF<sub>5</sub> gas is introduced into the reaction chamber for pre-fluorination for 1 h at room temperature to remove the remaining moisture adsorbed on the surface of the samples and metal inside the chamber. Prior to laser fluorination, all the remaining gases in the chamber are thoroughly evacuated ( $<10^{-4}$  mbar). Then, approximately 110 mbar of BrF<sub>5</sub> is introduced into the reaction chamber using an attached cold finger (Figure 2A). The amount of introduced BrF<sub>5</sub> is roughly two times greater than the stoichiometric requirement of a  $\sim 2$  mg silicate sample. We adopted two modes of laser power control for fluorination; manual mode and automated (Table 1). In the manual lasing mode, the laser output and positioning of the laser beam are manually adjusted, whereas in the automated lasing technique the position of laser beam is fixed and the diameter of laser beam and laser power are changed using the laser control functions in the laser system. At the beginning of operation in the

**TABLE 1** Mode of laser power control for fluorination

Power control mode	Beam size <sup>a</sup> (mm)	Reaction time <sup>b</sup> (min)	Laser power <sup>c</sup> (%)	Additional lasing <sup>d</sup>
Manual mode	<0.5	$\sim 10$	3 $\rightarrow$ 70	-
Automated mode I	>3.0	2–5	20 $\rightarrow$ 60	2–5 min in manual mode
Automated mode II	>2.5	2–5	10 $\rightarrow$ 60	
Automated mode III	>2.0	2–5	5 $\rightarrow$ 60	

<sup>a</sup>Beam sizes were checked by burning and melting test of wood and aluminum plates.

<sup>b</sup>The end of reaction was decided by there being no more glow in the sample holder.

<sup>c</sup>Generally, the initial laser power in the automated mode is increased as the beam size is reduced.

<sup>d</sup>Additional lasing with focused beam applied to ensure complete reaction. Completion of the reaction was decided by watching for no more glow in the sample holder.

automated mode, the sample is gradually heated at low laser power followed by gradual increase to 60%. Usually, most of the samples are decomposed at the end of the automated lasing mode. After the fluorination, unreacted grains, if remaining, are heated by reducing the beam size to  $\sim 0.5$  mm to complete the fluorination. The end of the reaction is decided by observing no further glow on a monitor connected to a CCD camera. This additional laser heating is performed on the sample fragments hidden at the edge of the sample holder.

All gaseous species from a sample are expanded into the first cryogenic trap to remove condensable gases such as excess BrF<sub>5</sub>, BrF<sub>3</sub> and SiF<sub>4</sub> at liquid nitrogen temperature ( $-196^{\circ}\text{C}$ ) for 7 min (Figure 1). Non-condensable F<sub>2</sub> gas, if any, is then allowed to pass through the KBr getter heated at  $150^{\circ}\text{C}$  in order to convert it into bromine ( $\text{F}_2 + 2\text{KBr} \rightarrow \text{Br}_2 + 2\text{KF}$ ) which is trapped in the second cryogenic trap 2 for 5 min. The resulting pure O<sub>2</sub> is finally collected on cryogenic trap 3 containing a pellet of 13X molecular sieve (MS13X) for 15 min at liquid nitrogen temperature (Figure 1). The oxygen yield is calculated from the O<sub>2</sub> gas pressure measured with a pressure transducer after desorption of the O<sub>2</sub> gas from the MS13X trap at room temperature. The volume of the cryogenic trap 3 and pressure transducer are calibrated using a known amount of CO<sub>2</sub> before attaching the transducer to the line. For the calibration the pellet of 13X molecular sieve in trap 3 is removed, as molecular sieve is known to adsorb CO<sub>2</sub> irreversibly. During a series of extraction and purification procedures, the line is maintained at approximately  $40^{\circ}\text{C}$  using heating tapes to minimize adsorption of gases on the inner wall of the metallic line.

### 3.2 | Mass spectrometer and conditions for oxygen isotope measurement

The gas source isotope ratio mass spectrometer equipped with a dual-inlet system is connected on-line to the laser fluorination system (Figure 1). In our system, oxygen gas (O<sub>2</sub>) is used as the analyte. The

oxygen gas desorbed from the MS13X in cryogenic trap 3 is expanded into a metal bellows in the dual-inlet system directly. For the  $^{17}\text{O}/^{16}\text{O}$  and  $^{18}\text{O}/^{16}\text{O}$  ratio analysis, we determine the beam intensity of the masses 32, 33, and 34 collected by Faraday cups connected to the resistors with  $\Omega = 3 \times 10^8$ ,  $3 \times 10^{11}$ , and  $1 \times 10^{11}$ , respectively. Isodat 3.0 software (Thermo Fisher Scientific) is used for data acquisition. Each measurement consisted of 10 cycles with an integration time of 26 s. The internal precision of  $\delta^{17}\text{O}$  measurements is  $<0.02\%$  (2SEM, standard error of the mean). The data shown in this paper is an average of duplicate measurements.

To check daily systematic bias and operating conditions of the mass spectrometer, so-called zero-enrichment analysis is performed by introducing the working standard  $\text{O}_2$  gas into both the sample and the reference bellows prior to the sample measurements. The zero-enrichment measurements typically showed less than 0.03% change in the  $\delta^{17}\text{O}$  and  $\delta^{18}\text{O}$  values, so we did not take the instrumental bias into consideration in later data handling. If a sample contains nitrogen compounds, fluorination may produce  $\text{NF}_3$  and the  $\text{NF}^+$  fragment ion ( $m/z$  33) forms in the ion source, overlapping the  $^{17}\text{O}^{16}\text{O}^+$  peak in the mass spectrum because the mass resolution of  $\sim 200$  of the mass spectrometer is much lower than the required resolution of  $\sim 4440$  ( $M/\Delta M$ ) for the separation of  $^{16}\text{O}^{17}\text{O}^+$  from  $^{14}\text{N}^{19}\text{F}^+$ . To obtain a precise  $^{17}\text{O}/^{16}\text{O}$  ratio of a natural sample, this isobaric interference at  $m/z$  33 must be considered.<sup>4</sup> Thus, we checked for the presence of  $^{14}\text{N}^{19}\text{F}_2^+$  and  $^{14}\text{N}^{19}\text{F}_3^+$  peaks at  $m/z$  52 and  $m/z$  71 after each analysis. The oxygen gases extracted from

typical silicate minerals, however, showed no recognizable peaks at these masses, indicating that their interference was negligible. In the case where samples contain a large amount of nitrogen, the interference of  $^{14}\text{N}^{19}\text{F}^+$  can be problematic.<sup>12</sup>

### 3.3 | Determination of $\delta$ -values for working standard $\text{O}_2$

The oxygen isotope ratios are generally expressed in  $\delta$ -notation relative to VSMOW (Vienna Standard Mean Ocean Water) where  $\delta$  is defined as the per mil (‰) deviation of  $^{17}\text{O}/^{16}\text{O}$  and  $^{18}\text{O}/^{16}\text{O}$  ratios of a sample from those of VSMOW, i.e.,  $\delta^{17}\text{O} = \{(^{17}\text{O}/^{16}\text{O})_{\text{sample}} / (^{17}\text{O}/^{16}\text{O})_{\text{VSMOW}}\} - 1$  and  $\delta^{18}\text{O} = \{(^{18}\text{O}/^{16}\text{O})_{\text{sample}} / (^{18}\text{O}/^{16}\text{O})_{\text{VSMOW}}\} - 1$ . However, we report both values relative to our 'working standard  $\text{O}_2$  (WST)' reference gas due to there being no direct calibration for the reference gas relative to VSMOW in this study (Table 2).

In an oxygen three-isotope plot, if the range of  $\delta^{17}\text{O}$  and  $\delta^{18}\text{O}$  values is large, the values do not fall on a straight line but on a slightly convex curve.<sup>18</sup> Therefore,  $\Delta^{17}\text{O}$ , the deviation of  $^{17}\text{O}/^{16}\text{O}$  ratios of samples from the fractionation line, is defined by a linear equation as  $\Delta^{17}\text{O} = \delta^{17}\text{O} - \lambda \times \delta^{18}\text{O} - \gamma$ , where  $\delta^{17}\text{O} = 10^3 \ln(1 + \delta^{17}\text{O})$  and  $\delta^{18}\text{O} = 10^3 \ln(1 + \delta^{18}\text{O})$ ,  $\lambda$  is a slope of mass-dependent fractionation line, and  $\gamma$  is the ordinate offset of the fractionation line.<sup>18</sup> To compare the deviation of  $^{17}\text{O}/^{16}\text{O}$  ratios of the reference samples

**TABLE 2**  $\delta^{17}\text{O}$ ,  $\delta^{18}\text{O}$  and  $\Delta^{17}\text{O}$  values of the reference samples obtained in automated and manual lasing modes

Sample	Lasing technique	No. of analyses	$\delta^{17}\text{O}_{\text{WST}}^{\text{a}}$			$\delta^{18}\text{O}_{\text{WST}}^{\text{a}}$			$\Delta^{17}\text{O}^{\text{b}}$			$\delta^{18}\text{O}_{\text{VSMOW}}^{\text{c}}$
			Avg. (‰)	SD ( $2\sigma$ )	SEM ( $2\sigma$ )	Avg. (‰)	SD ( $2\sigma$ )	SEM ( $2\sigma$ )	Avg. (‰)	SD ( $2\sigma$ )	SEM ( $2\sigma$ )	Avg. (‰)
Juan de Fuca	Automated III	6	8.006	0.079	0.032	15.340	0.168	0.069	0.001	0.016	0.007	5.593
Basalt glass	Automated II	3	8.000	0.110	0.064	15.326	0.231	0.134	0.002	0.011	0.006	5.579
	Automated I	36	8.017	0.105	0.018	15.353	0.195	0.033	0.005	0.020	0.003	5.606
	Manual	39	7.884	0.245	0.039	15.130	0.428	0.069	-0.010	0.047	0.008	5.384
UWG2 garnet	Automated III	17	8.129	0.059	0.014	15.579	0.094	0.023	-0.001	0.020	0.005	5.829
	Automated II	3	8.117	0.019	0.011	15.569	0.047	0.027	-0.008	0.009	0.005	5.820
	Automated I	4	8.145	0.049	0.024	15.586	0.043	0.022	0.011	0.027	0.013	5.836
	Manual	12	8.099	0.121	0.035	15.441	0.189	0.055	0.041	0.065	0.019	5.693
NBS28 quartz	Automated III	10	10.007	0.074	0.024	19.143	0.139	0.044	0.011	0.019	0.006	9.359
	Automated I	7	9.881	0.071	0.027	18.901	0.124	0.047	0.010	0.016	0.006	9.120
	Manual	10	9.620	0.212	0.067	18.423	0.379	0.120	0.000	0.020	0.006	8.646
San Carlos olivine	Automated III	9	7.946	0.093	0.031	15.200	0.161	0.054	0.014	0.021	0.007	5.455
	Automated I	6	7.834	0.056	0.023	14.981	0.125	0.051	0.017	0.026	0.010	5.238
	Manual	10	7.876	0.099	0.031	15.070	0.193	0.061	0.012	0.016	0.005	5.326
Obsidian (in-house)	Automated III	20	9.528	0.094	0.021	18.252	0.166	0.037	-0.002	0.025	0.006	8.477
	Automated II	2	9.516	0.021	0.015	18.212	0.095	0.067	0.006	0.028	0.020	8.437
	Automated I	6	9.500	0.023	0.009	18.190	0.042	0.017	0.002	0.017	0.007	8.415

<sup>a</sup> $\delta$ -values are expressed as a per mil relative to working standard  $\text{O}_2$  (WST).

<sup>b</sup> $\Delta^{17}\text{O} = 10^3 \ln(\delta^{17}\text{O}_{\text{WST}} + 1) - 0.528 \times 10^3 \ln(\delta^{18}\text{O}_{\text{WST}} + 1) + 0.065$ .

<sup>c</sup> $\delta^{18}\text{O}$  values relative to VSMOW are converted from the  $\delta^{18}\text{O}$  values relative to the working standard  $\text{O}_2$  by a conversion factor of 0.9904 ( $n = 24$ ) by assuming  $\delta^{18}\text{O}_{\text{VSMOW}} = 5.8\%$  for UWG2 garnet.<sup>29</sup>

SD = standard deviation; SEM = standard error of the mean

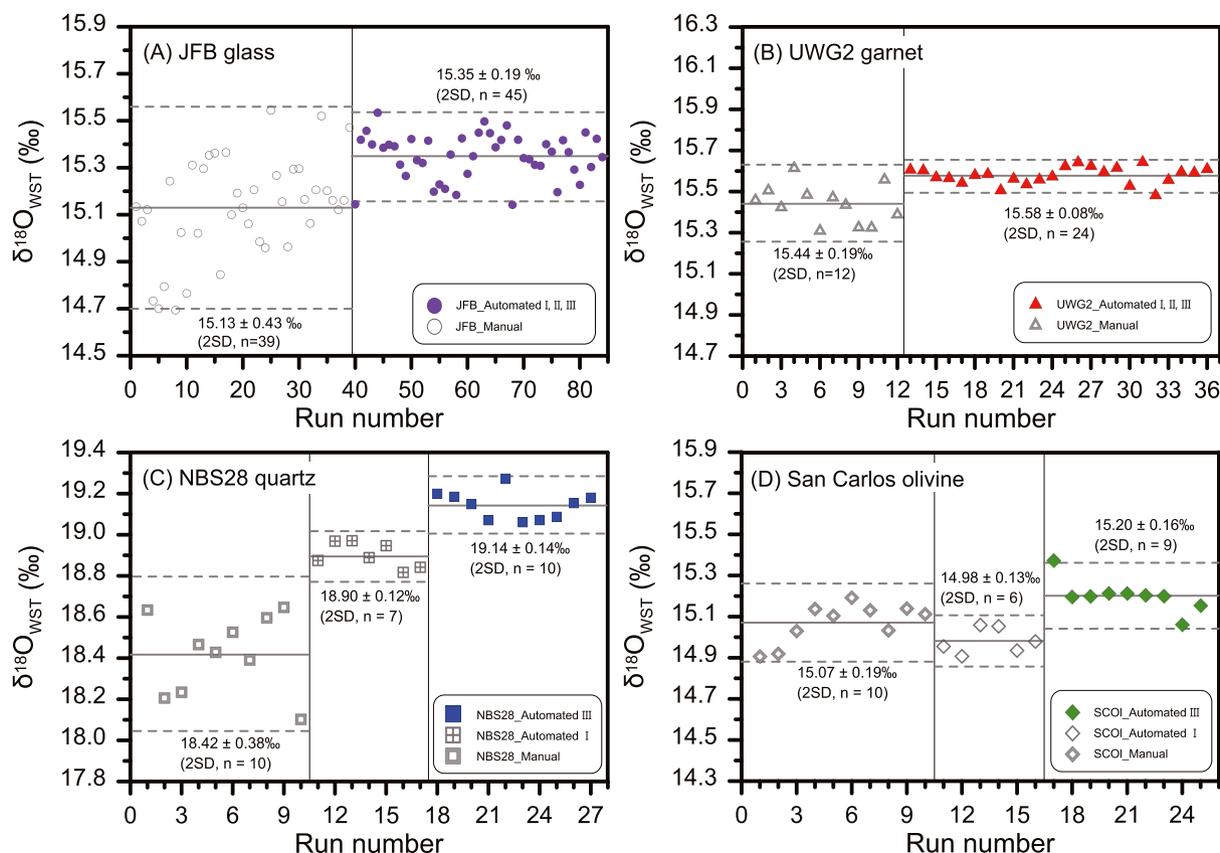
in this study, we report  $\Delta^{17}\text{O}$  values of the samples relative to UWG2 garnet. First, we defined the fractionation line for silicate materials from the regression of the  $\delta^{17}\text{O}_{\text{WST}}$  and  $\delta^{18}\text{O}_{\text{WST}}$  values in this study (Figure S1, supporting information). The regression equation is expressed as  $\delta^{17}\text{O}_{\text{WST}} = (0.528 \pm 0.002) \times \delta^{18}\text{O}_{\text{WST}} - (0.057 \pm 0.034)$ . The slope of 0.528 is in good agreement with those from other studies on terrestrial rocks and minerals.<sup>19–23</sup> The  $\Delta^{17}\text{O}$  values are calculated from  $\delta^{18}\text{O}_{\text{WST}}$  and  $\delta^{17}\text{O}_{\text{WST}}$  values and by assuming that  $\Delta^{17}\text{O}$  value of UWG2 garnet ( $n = 24$ ) is zero, where  $\lambda = 0.528$  and  $\gamma = -0.065$ . However, this approach can be used only for relative comparison of the samples in oxygen isotope analysis because we cannot assure that the oxygen isotope ratios of UWG2 garnet plot exactly on the fractionation line on the VSMOW scale. Furthermore, the slope of the fractionation line assigned by a measurement of terrestrial samples displays little difference among the sample collections.<sup>19–23</sup>

## 4 | RESULTS AND DISCUSSION

We repetitively analyzed the reference minerals to assess the analytical reproducibility. The results are summarized in Table 2. The individual  $\delta^{18}\text{O}$  values of the reference materials are shown in

Figures 3A–3D, where the data obtained in different analytical modes are grouped. The results of 200 individual oxygen isotope ratio measurements and the relevant analytical parameters (e.g., sample weight, oxygen yield, lasing mode, beam size, and reaction time) are given in the Table S1 (supporting information). In the following discussion, the reproducibility of the average  $\delta^{17}\text{O}$  and  $\delta^{18}\text{O}$  values is expressed as 2SD (2 times the standard deviation) unless mentioned otherwise.

The previous laser fluorination system at KOPRI used a 20 W  $\text{CO}_2$  laser with binocular optical system to observe the reaction.<sup>7</sup> The reaction chamber was manipulated manually on the XY-stage during laser irradiation with a highly focused beam. The analytical reproducibilities for the  $\delta^{18}\text{O}$  values of typical reference minerals such as UWG2 garnet, NBS28 quartz, San Carlos olivine and JFB glass (in-house standard sample at that time) were  $\pm 0.21\text{‰}$ ,  $\pm 0.29\text{‰}$ ,  $\pm 0.18\text{‰}$  and  $\pm 0.25\text{‰}$ , respectively.<sup>7</sup> Following the modification of the purification line with a new 25 W  $\text{CO}_2$  laser, we re-analyzed the same reference materials using the manual lasing mode which was the same as previously reported. The results neither reached a sufficient level of reproducibility nor were they in agreement with the recommended values (Figure 3). In particular, the JFB glass that has been used as our in-house reference showed a large isotopic variation. We initially thought

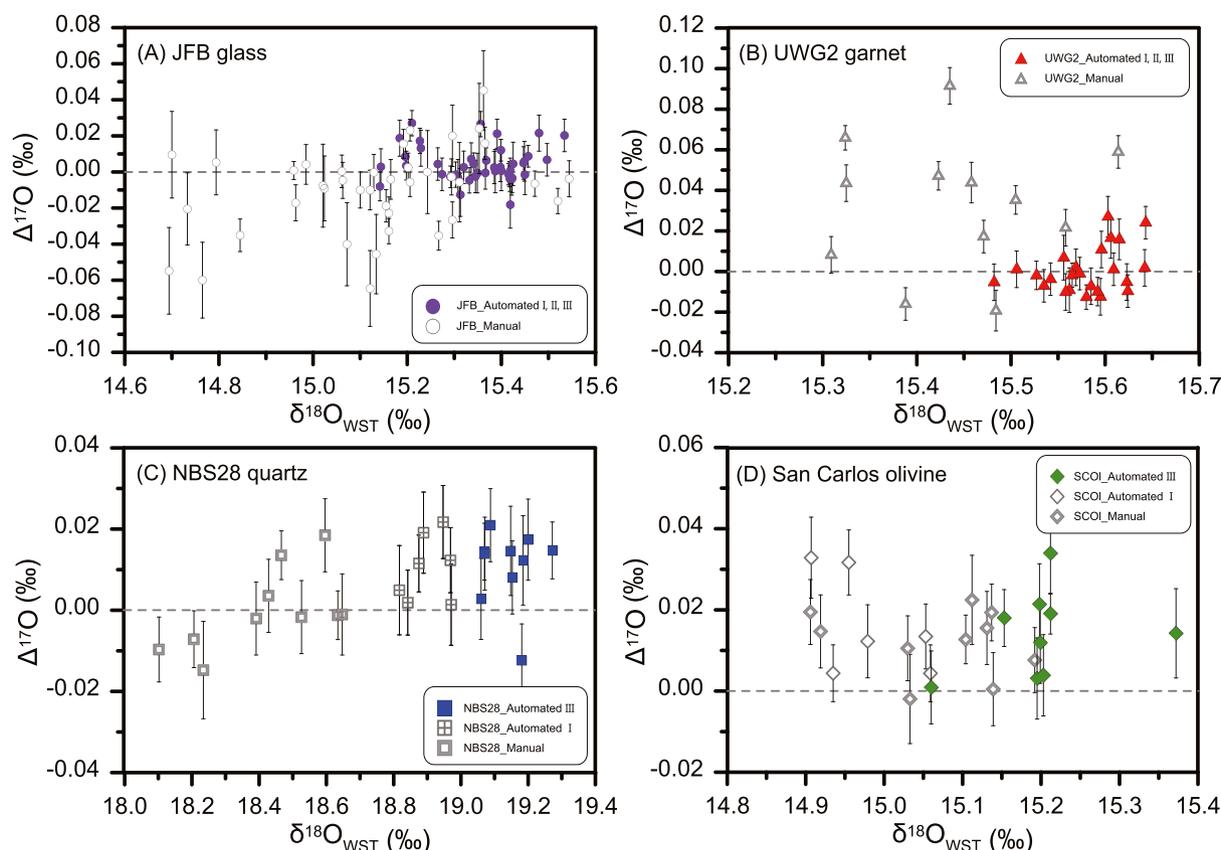


**FIGURE 3** Deviations of A, Juan de Fuca basalt (JFB) glass, B, UWG2 garnet, C, NBS28 quartz, and D, San Carlos olivine measurements by manual and automated laser techniques. Errors ( $2\sigma$ ) are within the size of the symbols in the plots. Averages are shown as gray solid lines and  $2\sigma$  standard deviations (SD) are shown as gray dashed lines. The automated lasing technique provides better precision than the manual lasing technique. Moreover, the quartz and olivine results obtained by the automated lasing technique are grouped by the size of the laser beam [Color figure can be viewed at [wileyonlinelibrary.com](http://wileyonlinelibrary.com)]

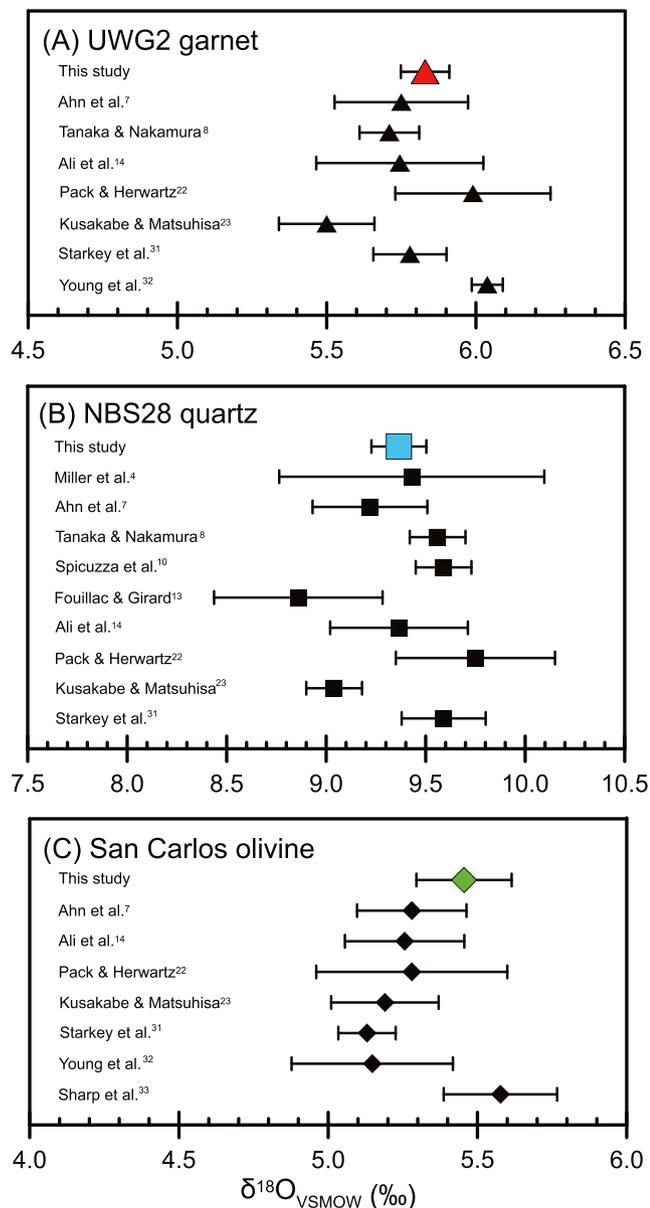
that the variation resulted from the presence of numerous olivine and plagioclase micro-phenocrysts because uneven distribution of the phenocrysts could have caused isotopic fractionation in the glass fragments (Figure S2, supporting information).<sup>24</sup> However, it was found that such micrometer-sized phenocrysts in the basalt glass do not affect the oxygen isotope variability (Table S2, supporting information). Instead we observed that the results of JFB glass obtained by the manual lasing technique can be grouped depending on who handled the laser system (Figure S3, supporting information); obvious operator bias was found. For this reason, we have introduced the automated lasing technique to minimize any unpredictable human error. The advantage of automated lasing is that a sample is irradiated uniformly using a defocused beam that covers the entire sample without changing the laser beam position (Table 1). The maximum diameter of the defocused beam used here was about 3 mm in the case of automated mode I. However, it proved difficult to react the sample completely with the 3 mm diameter beam due to the laser having too low an energy density. An oversized laser beam could influence samples in the neighboring holes. The minimum diameter of the defocused beam applied to our sample holder was 2 mm (automated mode III). We also tested an intermediately sized beam (2.5 mm diameter, automated mode II) to check if the isotopic fractionation depends

on the beam size. We used a maximum laser power of up to 60% during the automated lasing modes to prevent the BaF<sub>2</sub> window from cracking.

The three sub-methods of the automated lasing technique (automated modes I, II and III) were first applied to JFB glass, UWG2 garnet and obsidian to see whether the different energy density of the laser affects the isotopic results. These three materials did not show significant difference in the  $\delta^{18}\text{O}$  values obtained by the three automated lasing techniques (see Figures 3A and 3B, and Table 2). Thus, we decided to adopt automated mode III for further analyses. After adopting this technique, the reproducibility of all measurements was improved. It is noted that  $\delta^{18}\text{O}$  values of all tested samples increased consistently compared with the results obtained using the manual mode (Figure 3). However, the NBS28 quartz exhibited large variations in the  $\delta^{18}\text{O}$  value depending on the laser irradiation techniques (Figure 3C). It is known that 10.6  $\mu\text{m}$ -wavelength irradiation is well absorbed by quartz.<sup>2,10</sup> Figure 3C shows that this mineral exhibited low  $\delta^{18}\text{O}$  values with poor reproducibility when analyzed using the manual mode or low-density laser beam. The poor reproducibility was probably caused by either grain sputtering during lasing<sup>10,13</sup> or preferential vaporization of SiO<sub>2</sub>. Isotopic fractionation is associated with partial vaporization of SiO<sub>2</sub> molecules when they are irradiated at low temperatures.<sup>9,25</sup>



**FIGURE 4**  $\Delta^{17}\text{O}$  values of A, Juan de Fuca basalt (JFB) glass, B, UWG2 garnet, C, NBS28 quartz, and D, San Carlos olivine are plotted against  $\delta^{18}\text{O}$  values measured by manual and automated laser techniques.  $\Delta^{17}\text{O}$  values are calculated from  $\delta^{17}\text{O}_{\text{WST}}$  and  $\delta^{18}\text{O}_{\text{WST}}$  values. Gray dashed lines represent zero deviation of  $^{17}\text{O}/^{16}\text{O}$  ratio from the fractionation line. Error bars represent 1SEM [Color figure can be viewed at [wileyonlinelibrary.com](http://wileyonlinelibrary.com)]



**FIGURE 5**  $\delta^{18}\text{O}_{\text{VSMOW}}$  values by the automated lasing technique of A, UWG2 garnet, B, NBS28 quartz, and C, San Carlos olivine obtained in this study. The data for NBS28 quartz and San Carlos olivine were obtained by automated method III because the high-density laser can prevent isotopic fractionation during laser fluorination. Literature data are shown for comparison. The error bars represent  $2\sigma$  standard deviations [Color figure can be viewed at [wileyonlinelibrary.com](https://onlinelibrary.wiley.com)]

Depletion in  $^{18}\text{O}$  is caused by the difficulty of breaking the Si- $^{18}\text{O}$  bond at insufficient energy density, thus resulting in low  $\delta^{18}\text{O}$  values.<sup>9</sup> In this respect, a high-density beam and rapid heating are recommended to avoid isotope fractionation during quartz fluorination.<sup>8</sup> As shown in Figure 3C, analysis with a high-density laser beam prevents isotope fractionation possibly caused by vaporization on the sample surface.<sup>8-10</sup> For San Carlos olivine (Figure 3D), the results obtained by automated mode III show slightly lower reproducibility ( $\delta^{18}\text{O}_{\text{WST}} = 15.20 \pm 0.16\text{‰}$ ,  $n = 9$ ) than the data obtained by the manual lasing technique. The fluorination

products (e.g.,  $\text{MgF}_2$ ,  $\text{FeF}_2$ ) which absorb infrared radiation could inhibit complete reaction resulting in detectable isotopic fractionation by partial reaction.<sup>26,27</sup> The results of NBS28 quartz and San Carlos olivine indicate that the isotopic fractionation appears to depend on the lasing technique used (Figures 3C and 3D). It is noted that the  $\delta^{18}\text{O}$  values of the quartz and olivine samples increased with decreasing beam size (automated mode I  $\rightarrow$  III). These results imply that the use of a high-density laser leads to unfractionated isotopic ratios. Moreover, isotopic fractionation of  $^{17}\text{O}$  was also observed in the  $\delta^{18}\text{O}$  versus  $\Delta^{17}\text{O}$  plot (Figure 4). The  $\Delta^{17}\text{O}$  values measured by the manual lasing technique are more scattered than the other data obtained by the automated lasing technique, except for the San Carlos olivine.

For comparison between the  $\delta^{18}\text{O}$  values of the reference materials and literature data,  $\delta^{18}\text{O}$  values relative to working standard  $\text{O}_2$  are converted into the VSMOW scale by a conversion factor of 0.9904 (refer to Table S1, supporting information) using repetitive measurements of UWG2 garnet ( $n = 24$ ) and assuming  $\delta^{18}\text{O}_{\text{VSMOW}} = 5.8\text{‰}$  for UWG2 garnet.<sup>29</sup> Figure 5 shows the  $\delta^{18}\text{O}$  values of the reference materials obtained by the automated lasing technique and literature data obtained by the  $\text{CO}_2$ -laser fluorination method (see also Table S2, supporting information). The data for NBS28 quartz ( $\delta^{18}\text{O}_{\text{VSMOW}} = 9.36\text{‰}$ ,  $n = 10$ ) and San Carlos olivine ( $\delta^{18}\text{O}_{\text{VSMOW}} = 5.46\text{‰}$ ,  $n = 9$ ) were obtained by automated method III because a high-density laser can prevent isotopic fractionation during laser fluorination. The average  $\delta^{18}\text{O}$  value of NBS28 quartz is slightly lower than the recommended value ( $\delta^{18}\text{O}_{\text{VSMOW}} = 9.58\text{‰}$ ),<sup>30</sup> but it is in good agreement with other literature data.<sup>4,7,8,10,13,14,22,23,31</sup> The average  $\delta^{18}\text{O}$  value of San Carlos olivine is also in agreement with the margin of error of the literature data.<sup>7,14,22,23,31-33</sup> While it is still unclear why the isotopic variability of sample depends on the sample type and lasing technique, our results suggest that the automated laser control coupled by a defocused beam can provide satisfactory results with sufficiently high precision for the analysis of silicate minerals, and indicate that we can achieve good analytical reproducibility and minimize isotope fractionation by using the automated laser fluorination technique, i.e., rapid reaction with a high-density beam.

## 5 | CONCLUSIONS

We have measured the oxygen isotope compositions of reference minerals (UWG2 garnet, NBS28 quartz and San Carlos olivine) and in-house standards (MORB glass and obsidian). The system described herein enables us to measure the  $\delta^{17}\text{O}$  and  $\delta^{18}\text{O}$  values of silicate materials with high precision. The results obtained by the automated lasing technique show good reproducibility (2SD) of  $\delta^{17}\text{O}$  and  $\delta^{18}\text{O}$  values, which are  $\pm 0.06\text{‰}$  and  $\pm 0.08\text{‰}$  for UWG2 garnet,  $\pm 0.07\text{‰}$  and  $\pm 0.14\text{‰}$  for NBS28 quartz,  $\pm 0.09\text{‰}$  and  $\pm 0.16\text{‰}$  for San Carlos olivine,  $\pm 0.10\text{‰}$  and  $\pm 0.19\text{‰}$  for MORB glass and  $\pm 0.08\text{‰}$  and  $\pm 0.15\text{‰}$  for obsidian. The  $\Delta^{17}\text{O}$  values of samples also show high reproducibility ( $\pm 0.02\text{‰}$ , 2SD). It is emphasized that the automated

lasing mode with a high-density beam and a short irradiation time leads to much better precision and unfractionated oxygen isotope compositions than the manual lasing mode.

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## SUPPORTING INFORMATION

Additional supporting information may be found online in the Supporting Information section at the end of the article.

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